Mansoura University	Electronics & Comm. Engg. Dept.	
Electronics Circuits 2 Term 1 Exam	Jan. 22, 2014	
3rd year students	3 Hours	
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Answer the following 25 MCQs in the MCQ answer sheet in the answer booklet:

(for each correct answer, you get 3 marks for a total of 75 Marks)

(for each wrong answer, you get -1 mark) & (You get zero for unanswered questions)

- Q1 When a BJT is in saturation, the
- ① base current cannot increase
- ② collector to emitter voltage is maximum
- 3 collector current does not change with an increase in base current
- None of the above
- Q2 In Fig. 1, the dc load line will intersect the y-axis at
- ① 1 mA

3 1.67 mA

② 2.5 mA

④ 5 mA

- Q3 If you Thevenize the input voltage divider, the Thevenin resistance is
- \odot 6.67 k Ω

3 20 kΩ

 \odot 10 k Ω

 \oplus 30 k Ω

- Q4 A well-designed CC amplifier has
- ① current gain > 1

3 both of the above

② voltage gain > 1

none of the above

- Q5 The efficiency of a class A output stage amplifier is
- ① close to 100%

③ about 50%

② around 75%

- 4 less than 25%
- Q6 The conduction angle of the transistor of a class B output stage amplifier equals
- ① 90°

3 180°

2 between 90 & 180°

- @ 270°
- Q7 A class AB amplifier is designed to operate in the linear region
- ① for the whole input cycle
- 3
- ② for slightly more than ½ of the input cycle
- Q8 Crossover distortion (dead-zone) is present in
- class A output stage amplifier
- class B output stage amplifier
- Q9 The gain of the OP AMP shown in Fig. 2 is
- ① -10
- 2 1
- ③ 10
- 4 11
- Q10 For the OP AMP in Fig.2: If Vin = 1V, the approximate value of Vout is
- ① 1V
- ② 10V
- ③ 5V
- 4 11V

- 3 for exactly ½ of the input cycle
- 4 for slightly less than 1/2 of the input cycle

5 V

PDC =

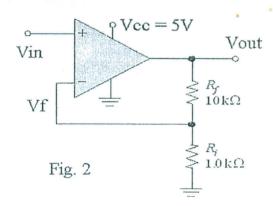
 $1 k\Omega$

200

20 kΩ

 R_2 10k Ω

- ③ class AB output stage amplifier
- none of the above



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- Q11 The input impedance of a noninverting amplifier is
- nearly 0 ohms
- (2) approximately equal to Ri
- approximately equal to Rf
- 4 extremely large
- Q12 In Fig. 3: the signal at node 1 is
- 1 DC level
- square wave 2
- (3) triangle wave
- series of +ve and -ve pulses
- Q13 In Fig. 3: the signal at node 2 is
- 1 DC level
- 2 square wave

3 triangle wave

positive feedback

- series of +ve and -ve pulses
- Q14 Hysteresis is incorporated in a comparator by adding
- a capacitor in series with the input
- 2 capacitors from the power supply to ground
- Q15 A comparator output can be limited (bounded) by
- reversing the power supply voltages
- decreasing the input resistance
- connecting the inverting input to ground Q16 When an instrumentation amplifier uses guarding, the shield is driven by a
- low-impedance differential source
- low-impedance common-mode source
- Q17 A typical instrumentation amplifier has
- high CMRR
- unity gain

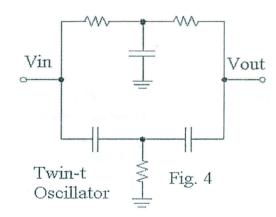
- 3 high-impedance differential source
- 4 high-impedance common-mode source

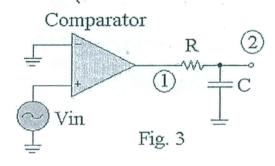
3 a small resistor in series with the input

3 putting a zener diode in a feedback path

- ③ low input impedance
- all of the above
- Q18 An application where an isolation amplifier is particularly useful is when
- 1 the input signal has very large dynamic range
- control of the freq. response is necessary
- Q19 The filter in Fig. 4 is a
- 1 low-pass filter
- 2 high-pass filter
- 3 band-pass filter
- 4 notch filter
- Q20 An example of an LC feedback oscillator is a
- Colpitts oscillator
- Wien-bridge oscillator 2
- 3 phase-shift oscillator
- (4) relaxation oscillator

- 3 voltages could present a hazard
- all of the above





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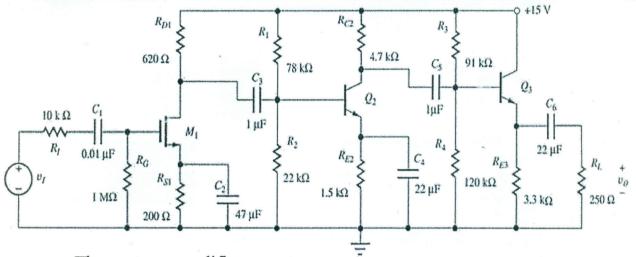
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Three-stage amplifier

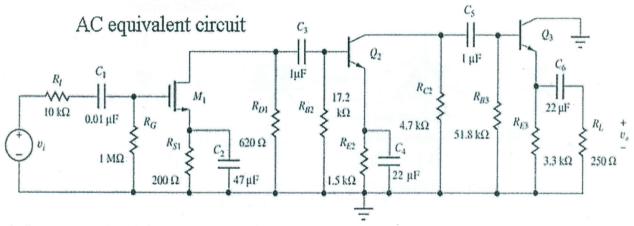


TABLE 17.3
Transistor Parameters

$arphi_{m}$, which is the $arphi_{m}$, which is the $arphi_{m}$, which is the $arphi_{m}$	ro Bo	Ccc/C- Cc	1/f
0.//		-03/-1 -01	ν γ - μ
M 10 ms	12210	5 5 5	~F 0.0
20 m3	12.2 K32 CC	o pr	DL 0.22
			The common property of the property
O ₂ 6/8 mS 2 39 kΩ	542 kQ 150	39 nF	nF 250 O
			1.1
0 706 0 1001-0	24.41.0 00	FO T	T 0500
Q3 79.0 IIIS 1.00 K22	24.4 K22 80	30 pr 1	DF 250 \$2
and the second second control of the second		CONTRACTOR OF THE PROPERTY OF	· Annual Control of the Control of t

TABLE 14.19

Q-Points

	Q-POINT VALUES
M_1	(5.00 mA, 10.9 V)
Q_2	(1.57 mA, 5.09 V)
Q_3	(1.99 mA, 8.36 V)

the lower-cutoff frequency for a network having n coupling and bypass capacitors can be estimated from

$$\omega_L \cong \sum_{i=1}^n \frac{1}{R_{iS}C_i} \tag{17.33}$$

in which R_{tS} represents the resistance at the terminals of the ith capacitor C_i with all the other capacitors replaced by short circuits. The product $R_{tS}C_i$ represents the short-circuit time constant associated with capacitor C_i .

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Q21 Fig. 5 is

Wien-Bridge Oscillator

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- 2 Phase-shift oscillator
- 3 Relaxation Oscillator
- Hartley Oscillator
- Q22 In a crystal oscillator, the crystal acts like a
- band-pass filter
- resonant circuit 2
- notch filter 3
- power source
- Q23 A bidirectional thyristor is the
- 4-layer diode
- SCR

3 triac

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silicon-controlled switch







Fig. 5

Fig. 6 (c) (b)

(d)

- Q24 The symbol for a silicon-controlled switch is shown in Fig.
- 6 (a)

3 6(c)

② 6(b)

- 4 6 (d)
- Q25 A programmable unijunction transistor (PUT) is programmed by choosing the
- RC time constant

3 power supply voltage

gate resistors

cathode resistor

Answer the following question:

(25 Marks)

- R1 Using the Short-Circuit Time-Constant (SCTC) method: For the multi-stage amplifier stage shown in the following figure
- a- Calculate R1S, R2S, R3S, R4S, R5S, and R6S in Ohms (12 Marks)
- Then estimate the lower cutoff frequency of the three-stage amplifier, $\omega_{\,\text{L}}$

(3 Marks)

.Repeat (a) for the same circuit after removing capacitors C2 and C4 (10 Marks)